



# THE ROLE OF THE FLOW FIELD GENERATED BY THE VENTING PROCESS ON THE PRESSURE TIME HISTORY OF A VENTED DEFLAGRATION



Martino Schiavetti, Tommaso Pini, Marco Carcassi

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**PERTURBATIONS**

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GENERATED BY THE VENTING PROCESS  
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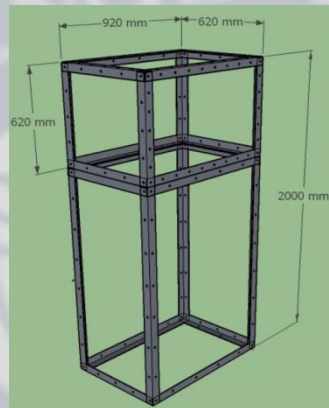
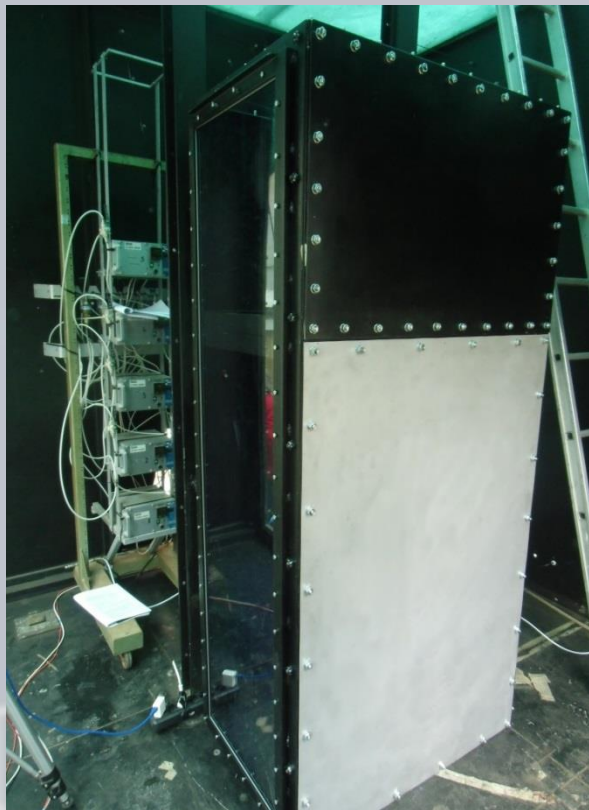
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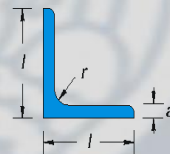
## Presentation overview:

- Experimental set-up (video recording)
- Perturbation originated by the two pivotal moments in vented deflagrations:
  - Vent opening
  - Flame front reaching the vent

## Experimental set-up



Height - 2000 mm  
Width - 920 mm  
Depth - 620 mm



$l = 50 \text{ mm}$   
 $a = 4 \text{ mm}$

Vent  
dimensions  
 $b = 500 \text{ mm}$   
 $c = 800 \text{ mm}$

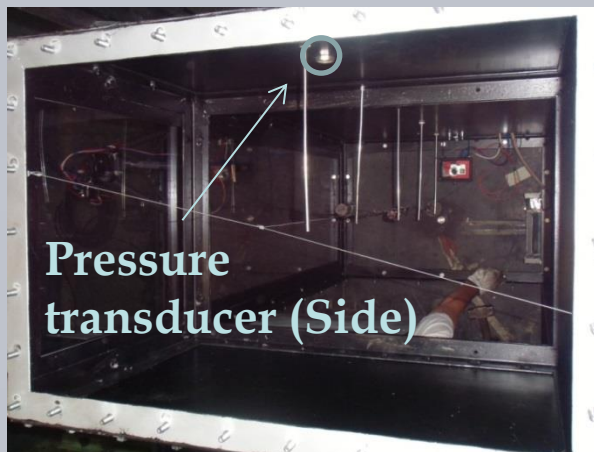


## Experimental set-up

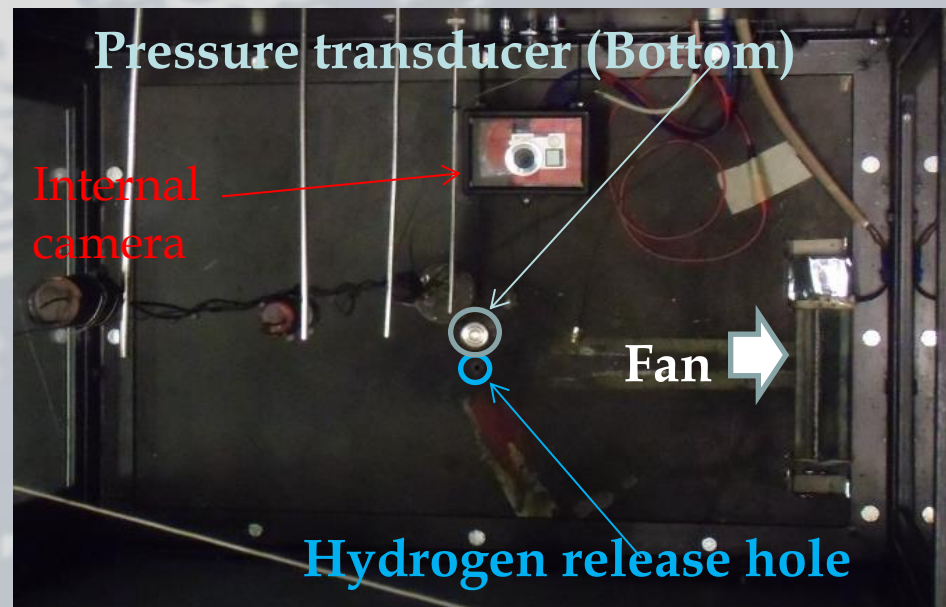
Pressure transducers:

Bottom: Center of the floor

Side: On the centerline of the back plate 1.5 m above the floor



External camera





# Experimental set-up

## 5 Sampling locations

Ignition location:

**Bottom:**

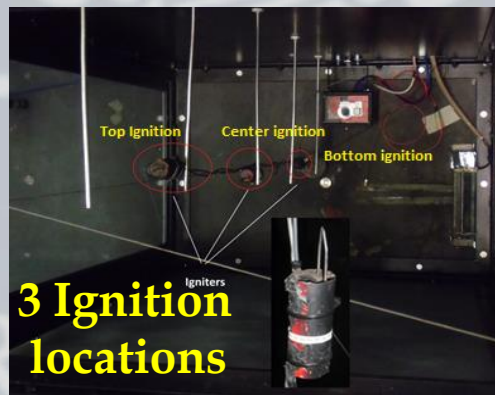
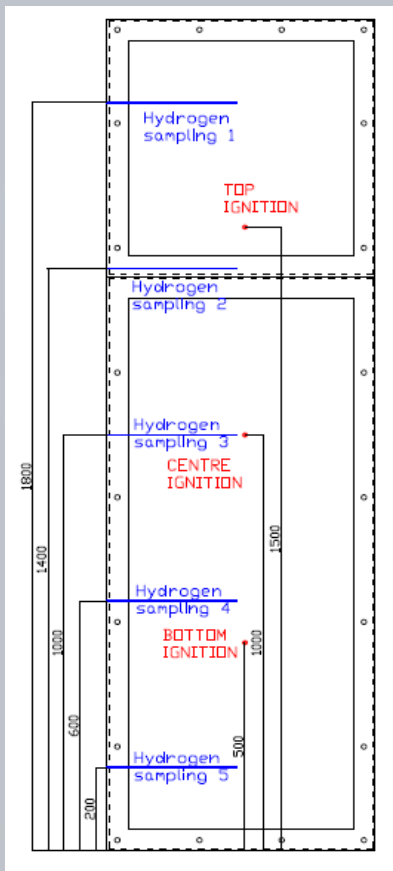
On the centerline 0.5m above the floor

**Centre:**

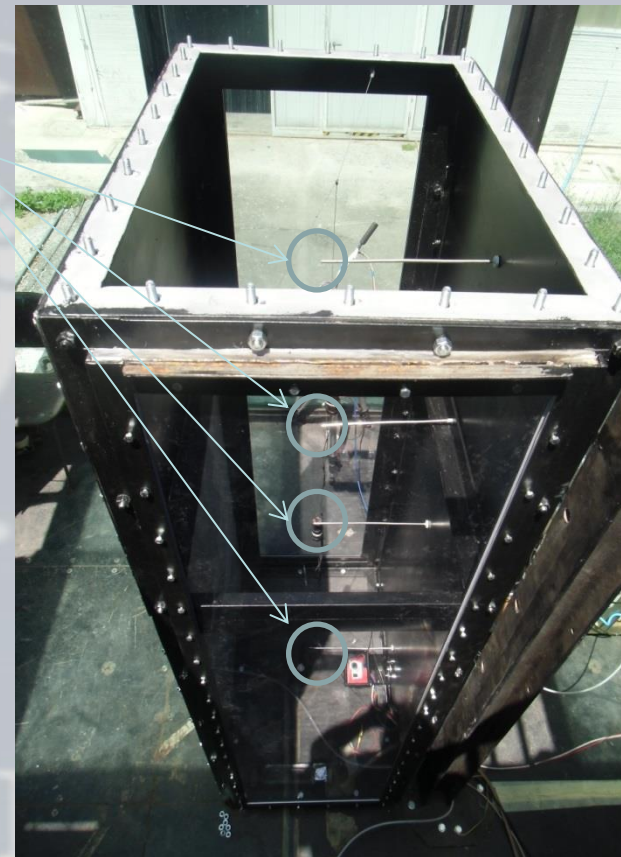
On the centerline 1m above the floor

**Top:**

On the centerline 1.5 m above the floor



**3 Ignition locations**



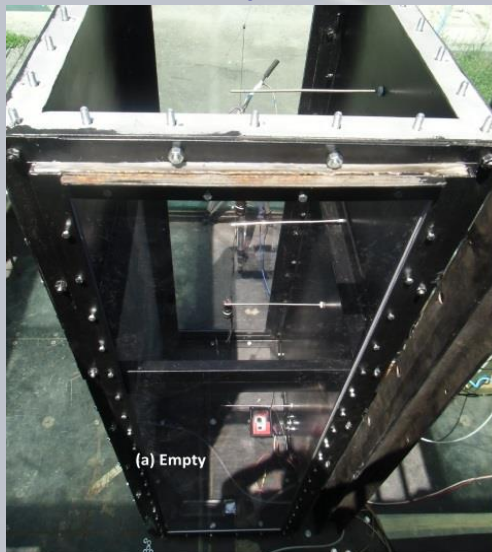
## Experimental set-up

### Internal obstacle configuration

Empty SSE

1 bottle

3 bottles



Free volume~1.141 m<sup>3</sup>



Free volume~1.085 m<sup>3</sup>

Volume reduction 4.86%

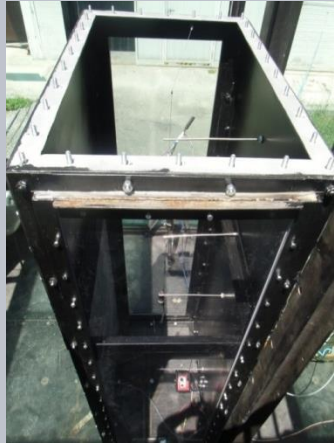


Free volume~0.974 m<sup>3</sup>

Volume reduction 14.58%

## Experimental set-up

Top vent



Front vent

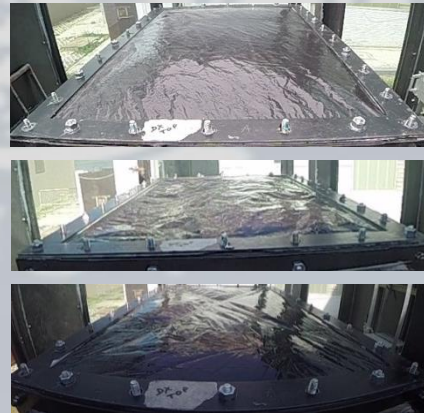


Vent type

Plastic sheets

FIKE vents

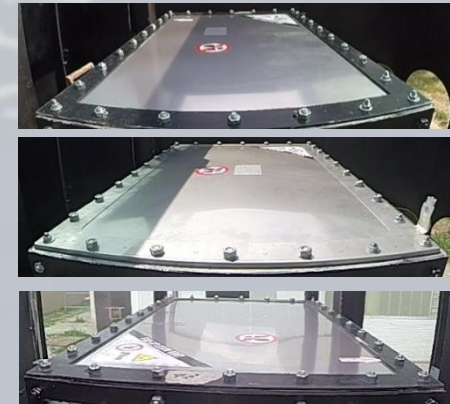
Vent locations



1

2

3



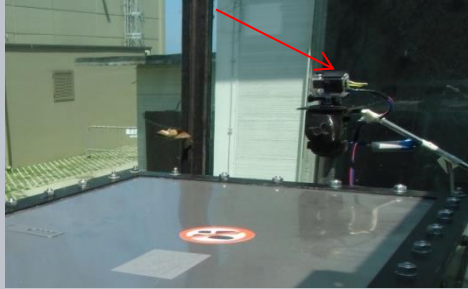
1

2

3



External camera

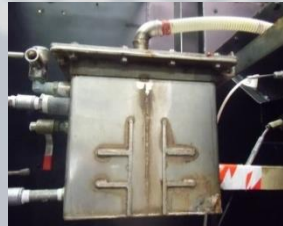


## Experimental set-up

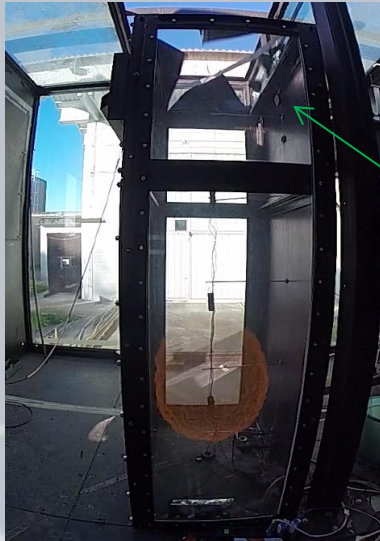
### Video recording

Video recording was performed at **240 fps** (frames per second)

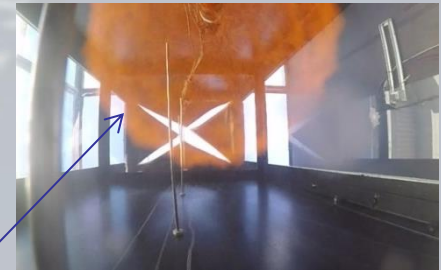
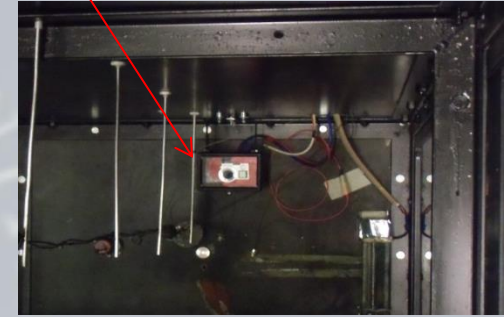
### Salt water spray injection system



Spray injection location



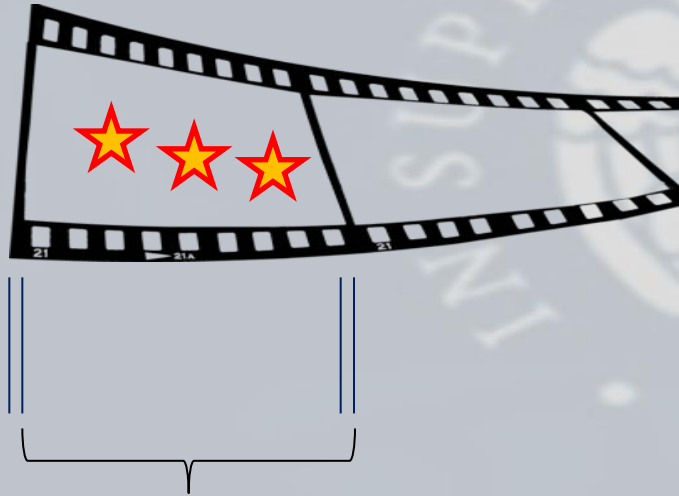
Internal camera



Visible Emission Spectra Sodium Chloride

## Experimental set-up

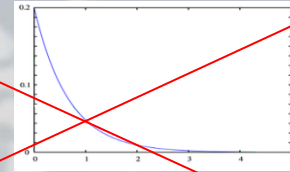
Video recording : Synchronization with pressure/time history



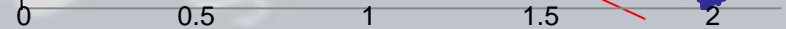
$$T_r + T_s = 1/240 \text{ s} = 4.17 \cdot 10^{-3} \text{ s}$$



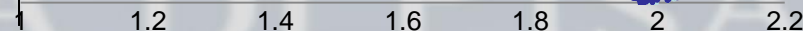
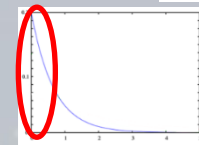
Ignition delay



Camera delay (signal transmission + internal circuits)

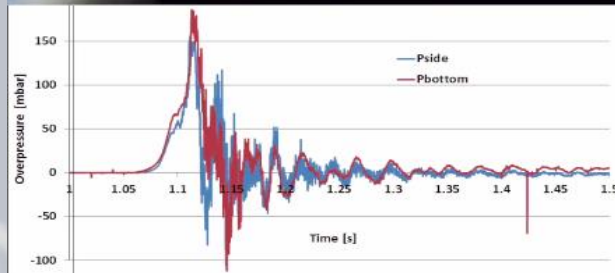


Only for tests with minimum ignition delay



# Experimental set-up

## Video recording : Synchronization with pressure/time history



Test TP52

Average concentration  
17.7% vol.



Video has been slowed down 10 times

## Pivotal moments in vented deflagrations

Every vented deflagration involve two crucial moments:

- **Vent opening**
- **Flame reaches the vent**

Both of these pivotal moment modify the boundary condition in which the flame front is developing and trigger perturbations.

### Vent opening:

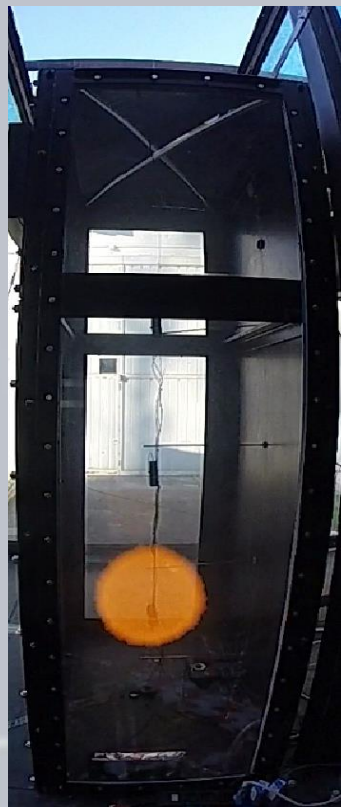
- Introduces perturbations generated by the  $dP$  at the vent surface which in turn originate a flow field directed towards the vent area
- Changes the distribution of the forces applied to the flame front by the expansion of the combustion products inside the «flame bubble»

### Flame front reaches the vent area:

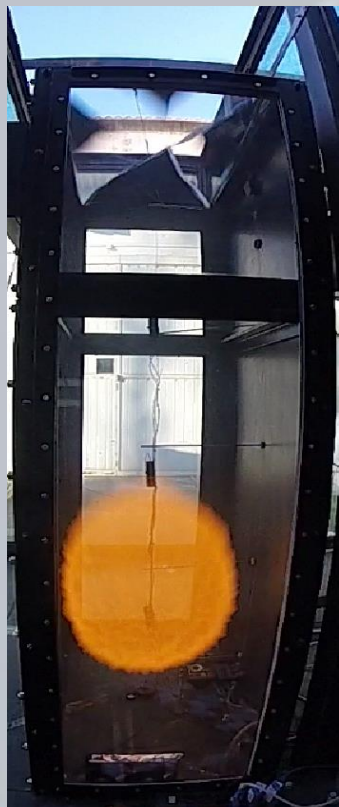
- Introduces perturbations generated by the sudden increase of the  $dV/dt$  at the vent surface which in turn originates perturbations
- The generated combustion products are removed towards the vent area and do not contribute anymore to the acceleration of the flame front (flame tends to become “quasi-stationary”)



## Vent opening:



Frame 584 (TP73)

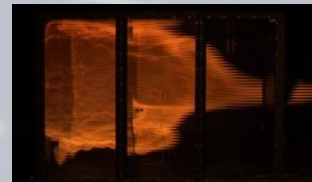


Frame 587 (TP73)



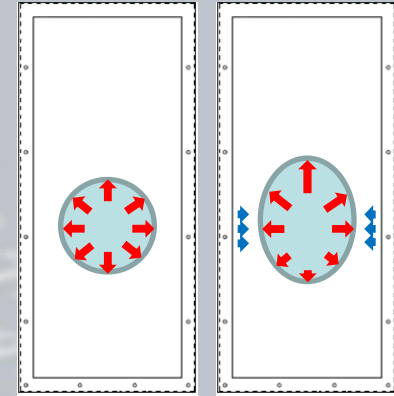
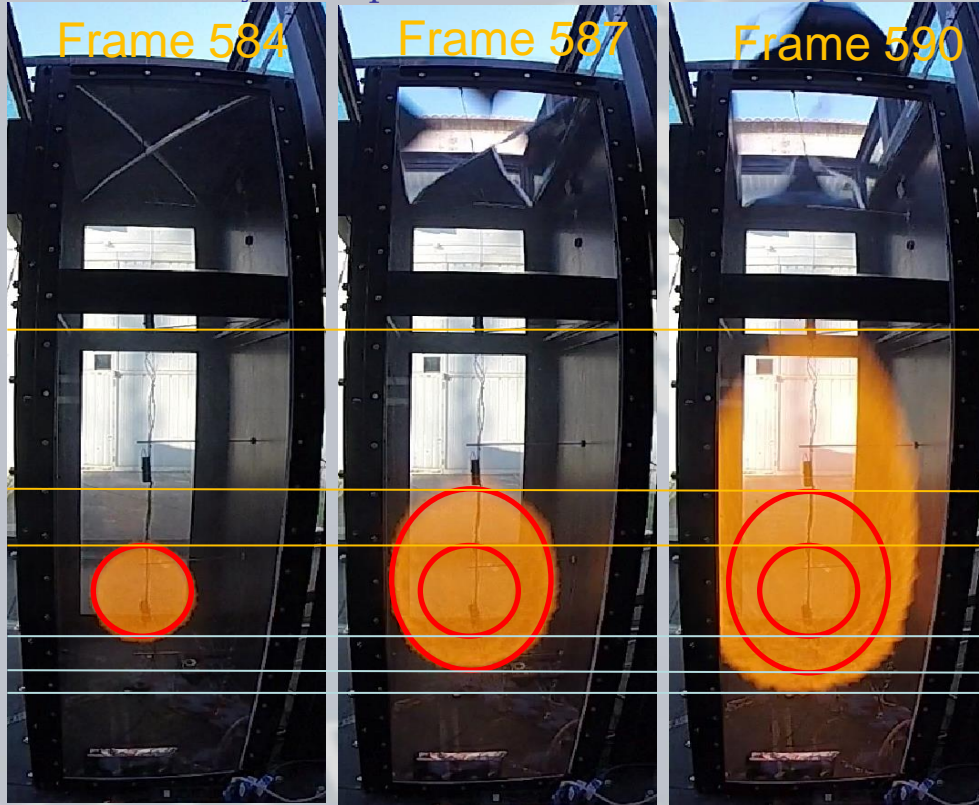
Frame 590 (TP73)

1. Introduces perturbations (accelerations) generated by the  $dP$  at the vent (The flame front is accelerated outwards by the expansion of the combustion products, so the effect of the superimposed "acoustic" accelerations is negligible)
2. Originate a flow field directed towards the vent area



3. Changes the distribution of the forces applied to the flame front by the expansion of the combustion products inside the «flame bubble»

Vent opening: Provokes changes the distribution of the forces applied to the flame front by the expansion of the combustion products



Velocity of the flame front increasing  
Flame front travels 0.5 to 0.6 m  
in 1 frame  $12.5 \cdot 10^{-3}$  s  
~40 m/s

Velocity of the flame front decreasing

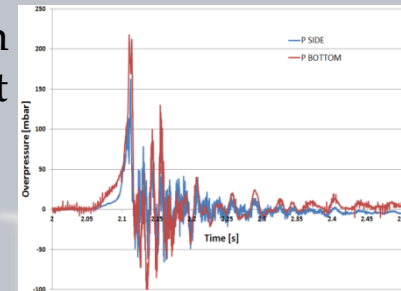
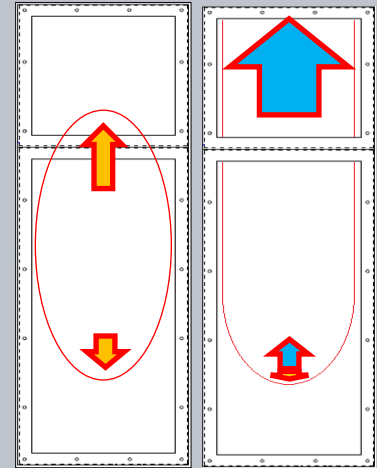
Test TP73 (18%vol)

## Flame front reaching the vent area:

1. Introduces perturbations (accelerations) generated by the sudden change of  $dV/dt$  at the vent (Such perturbation travel at the speed of sound)
  1. Helmholtz oscillations
  2. Acoustic response of the chamber
2. Combustion products generated inside the «flame bubble» direct mostly towards the vent area and do not contribute anymore to the acceleration of the flame front in outward direction (Flame front behaves like a free standing flame)



Frame 594 (TP73) Frame 595 (TP73)





## Flame front reaching the vent area: accelerations

Test TP55: H<sub>2</sub> average conc. 17.8%



The abrupt increase of the flow out of the vent area is responsible for the discontinuity that generates the acoustic response of the chamber:

1. Helmholtz oscillations
2. Acoustic response of the chamber

$$\frac{dV}{dt} = C_d \cdot A_v \cdot (2\Delta P / \rho)^{\frac{1}{2}}$$

**Distance traveled by perturbation (acceleration) 1.8 m**

**Time  $\leq 1$  frame =  $1/240\text{s} = 4.17 \cdot 10^{-3}\text{s}$**

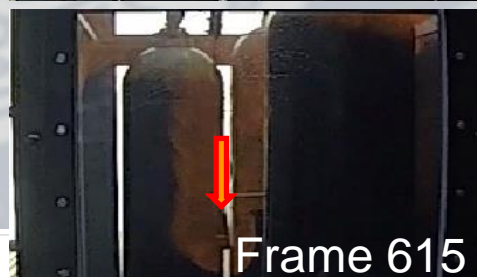
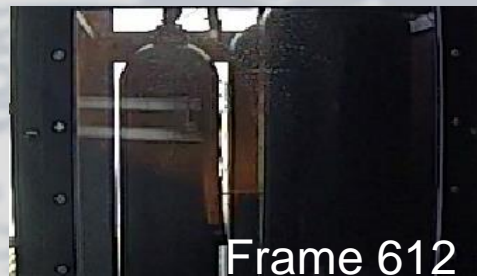
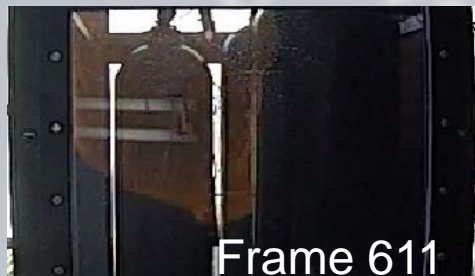
$$v_p \geq \frac{1.8\text{m}}{\frac{1}{240}\text{s}} \geq 432 \frac{\text{m}}{\text{s}}$$

Compatible with a perturbation travelling with the speed of sound in the combustion products

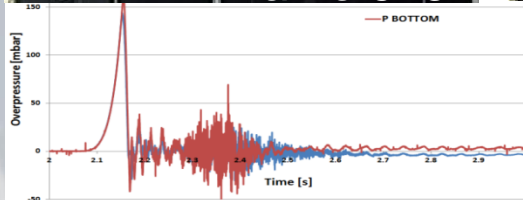




## Flame front reaching the vent area: flow field affecting the flame front opposite the vent



Combustion products generated inside the «flame bubble» are sucked towards the vent area, the generated flow field drags the flame front towards the vent, the flame “survives” only in regions where the velocities are lower.



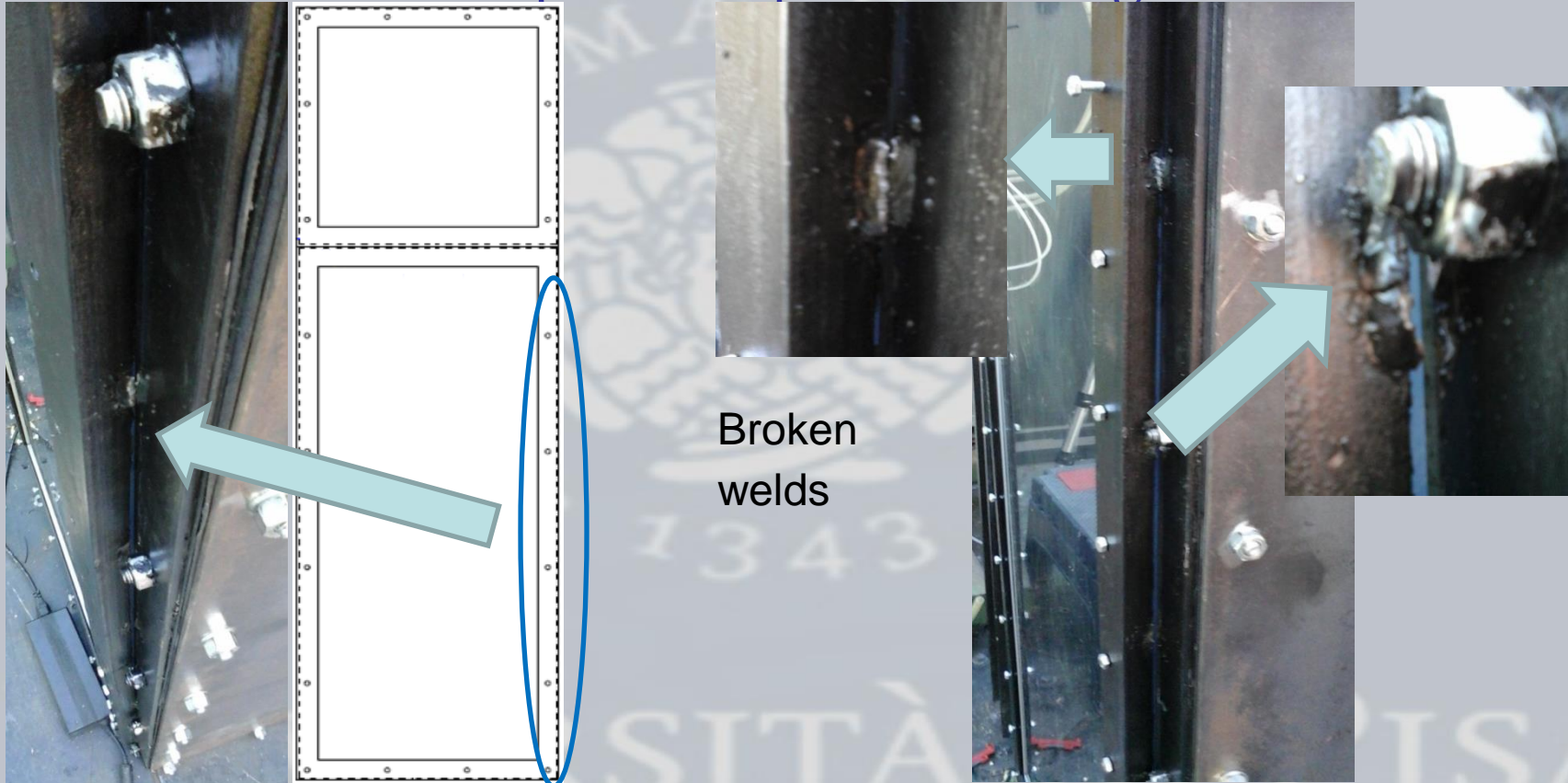
## Local pressure peaks: flow field around obstacles

Test TP55: H<sub>2</sub> average conc. 17.8%  
3 bottles – Top vent

Test TP52: H<sub>2</sub> average conc. 17.7%  
3 bottles – Front vent

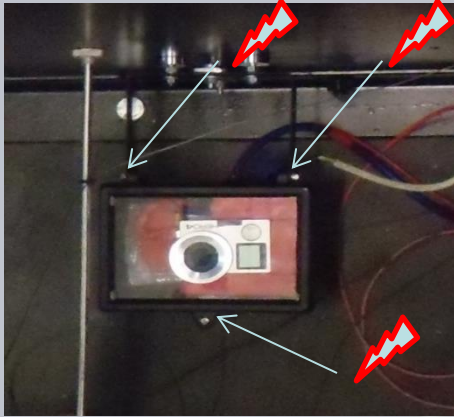


## Local pressure peaks: damages



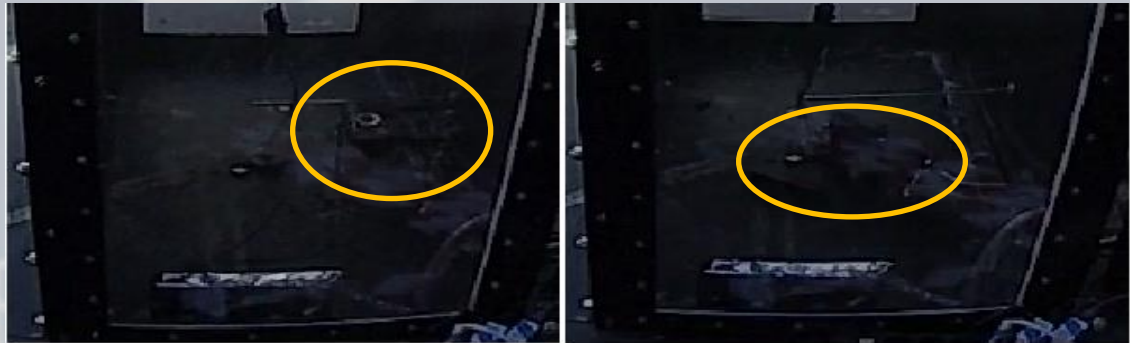


## Local pressure peaks: damages



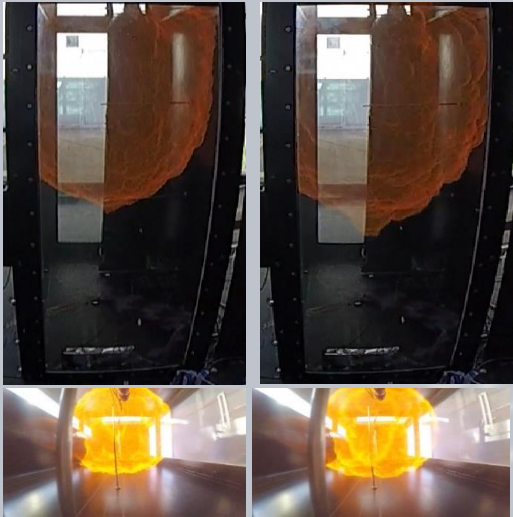
Camera protection case cap removed  
(broken hinges and closure – aluminum)

Displaced camera





## Acoustic oscillations



Frames

601

517

Frames

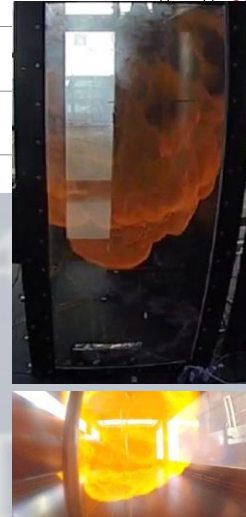
605

521

Frames

609

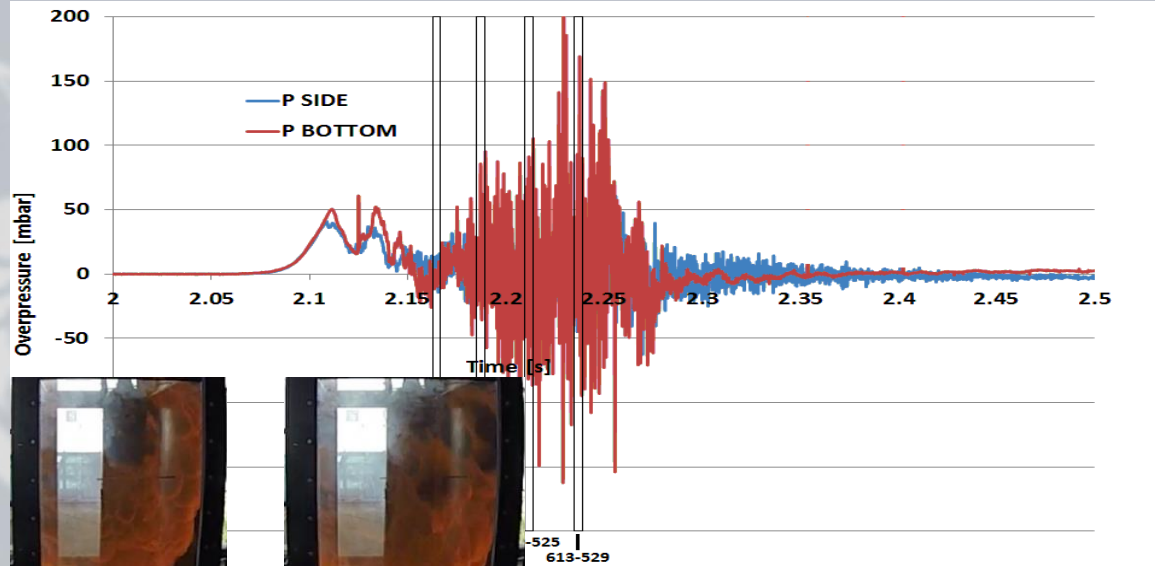
525



Frames

613

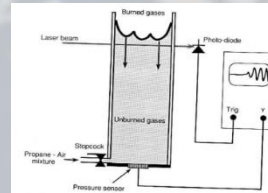
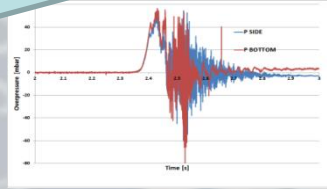
529



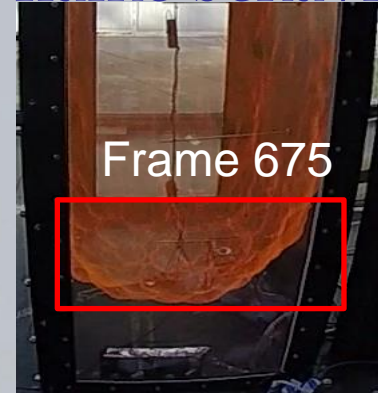
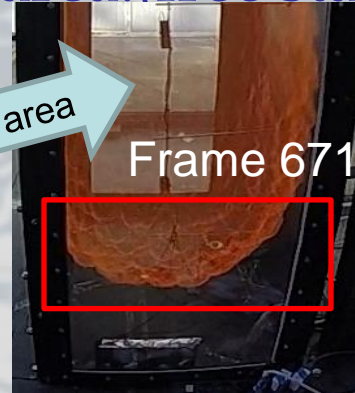
# Flame front reaching the vent area:(free standing flame behavior after venting)

Test TP74  
(14.3%vol.)

Flame front before reaching the vent area



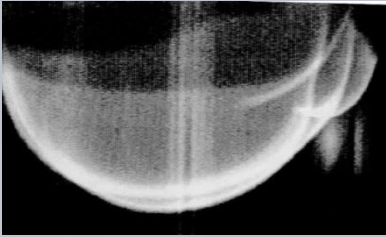
Geometrical analogy with the experimental set-up of Searby (Acoustic instabilities in premixed flames -Comb. Science and Tech. 1992 Vol.81)



Progressive changes in the flame shape after the flame front reaches the vent area



## Flame front reaching the vent area:(flame shape during last phase of deflagration)



Luminous emission from spontaneously curved flames in the absence of acoustic instabilities

“The flame typically has a curved shape with large “soft” cells generated by Darrieus-Landau instabilities”

G. Searby (Acoustic instabilities in premixed flames -Comb. Science and Tech. 1992 Vol.81)



# HySEA CONSORTIUM

GEXCON

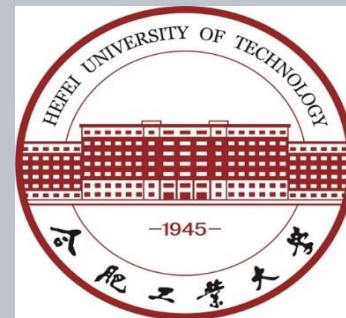


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# ACKNOWLEDGEMENTS

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THANK YOU  
For your attention

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