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Passive ventilation of enclosures with one vent, the uniformity criterion, and validation of pressure peaking phenomenon (unignited releases)

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Outline

- Natural and passive ventilation
- The model and the nomogram for steady state hydrogen concentration in an enclosure with one vent (sustained leak)
- The criterion for mixture uniformity during leak in an enclosure with one vent
- The model and the nomogram for leak flow rate limit leading to 100% hydrogen accumulation in an enclosure with time
- Validation of pressure peaking phenomenon

Ventilation



- Natural ventilation equations for air ventilation in buildings are derived in the assumption of equality of flow in and out of the enclosure (neutral plane is at the half of a vent height).
 - Passive ventilation: neutral plane for lighter than air gases can be anywhere below the half of a vent height.

Neutral plane location





Mole fraction X: natural vs passive

Natural ventilation:

$$X = \left[\frac{Q_0}{C_D A(g'H)^{1/2}}\right]^{2/3}$$

Passive ventilation:

$$X = f(X) \cdot \left[\frac{Q_0}{C_D A(g'H)^{1/2}}\right]^{2/3}$$

Difference:
$$f(X) = \left(\frac{9}{8}\right)^{1/3} \cdot \left\{ \left[1 - X\left(1 - \frac{\rho_{H_2}}{\rho_{air}}\right)\right]^{1/3} + (1 - X)^{2/3} \right\}$$

Safety design: natural or passive?

Difference:
$$f(X) = \left(\frac{9}{8}\right)^{1/3} \cdot \left\{ \left[1 - X\left(1 - \frac{\rho_{H_2}}{\rho_{air}}\right)\right]^{1/3} + (1 - X)^{2/3} \right\}$$



Natural ventilation equation (compared to passive): 7

- Underestimate x2 (lean)
- Overestimate x2 (rich)

Validation tests with helium (CEA)

- Experiments were carried out by CEA (France) in the enclosure with sizes HxWxD=1.26x0.93x0.93 m.
- One vent located on a wall near the ceiling.
- Three different vent sizes were studied:
 - Vent (a) WxH=90x18 cm,
 - Vent (b) 18x18 cm,
 - Vent (c) 90x3.5 cm.

Release of helium was directed upward from a tube located centrally 21 cm above the floor with internal diameter either 5 mm or 21 mm.

✤ Release rates ranges 5÷300 NI/min.

Predictions vs experiment C_{max}

Natural ventilation with "tuned" $C_D = 0.25$ - dashed lines. **Passive** ventilation equation with $C_D = 0.60$ solid lines.



Experiments





Nomogram (concentration C_{max})



Calculation example: 1.Release rate (1 g/s) 2.Vent Height (0.5 m) 3.Vent width (1 m) 4.Function curve 5.Concentration (13.7%)

Release limit (100% H2 accumulation)

Depending on the release rate and vent size there can be 100% of hydrogen accumulation in the enclosure.



Equation gives the lower limit of release flow rate that leads to 100% of hydrogen accumulation in enclosure.

(This limit has to be exceeded to have the pressure peaking phenomenon – see in following slides)

Nomogram: 100% accumulation

Example of use: sustained release of hydrogen 3 g/s in enclosure with a vent of W=0.3 m and H=0.07 m

will lead to 100% accumulation.

No dependence on enclosure volume (only accumulation time will depend).

Reproduces previous nomogram at C_{max} =100%



Pressure peaking phenomena

Small garage *LxWxH*=4.5x2.6x2.6 m ("brick" vent). Mass flow rate 390 g/s (350 bar, 5.08 mm orifice).



Solution: decrease PRD orifice size (and at the same time increase fire resistance of onboard storage)

Pressure peaking phenomena

Small garage *LxWxH*=4.5x2.6x2.6 m ("brick" vent). Mass flow rate 390 g/s (350 bar, 5.08 mm orifice).



Pressure peaking: validation

Formula for the pressure peaking calculation had been validated against experimental result obtained by KIT for the steady state release.



Conclusions

- The analytical model for uniform concentration in an enclosure with one passive vent for sustained leak is developed, validated, and used to build engineering nomograms.
- The criterion for mixture uniformity in a vented enclosure is suggested.
- The nomogram to calculate the mass flow rate limit leading to 100% gas concentration in the enclosure as a function of the vent width and height is developed (flow rate should be above this limit to apply the pressure peaking phenomenon calculations).
- Experiments with release of air, helium and hydrogen performed by KIT proved the existence of pressure peaking phenomena (PPP).
- It can be concluded that the PPP is essential part of hydrogen safety engineering (HSE) for all indoor use of HFC systems.
- It is recommended that value CD=0.6 is accepted for HSE as a conservative one.



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MSc in Hydrogen Safety Engineering (distance learning course):

http://www.ulster.ac.uk/elearning/programmes/view/course/10139

Fundamentals of Hydrogen Safety Engineering

(free download eBook, www.bookboon.com, 2012)